# DYNAMIC MEASUREMENTS OF COMMERCIAL HIGHWAY VEHICLES (WEIGHING-IN-MOTION)



#### NOTICE

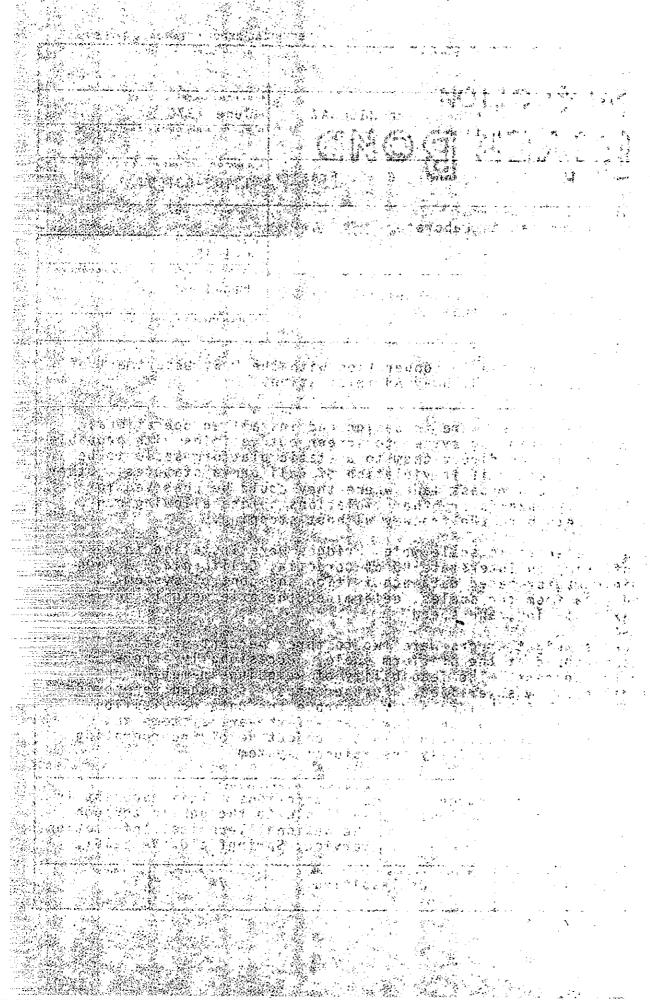
The contents of this report reflect the views of the Office of Transportation
Laboratory which is responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the State of California or the Federal Highway Administration.

This report does not constitute a standard, specification, or regulation.

Neither the State of California nor the United States Government endorse products or manufacturers. Trade or manufacturers' names appear herein only because they are considered essential to the object of this document.

	TECHNI	CAL REPORT STANDARD TITLE PAGE		
1 REPORT NO.	2. GOVERNMENT ACCESSION NO.	3. RECIPIENT'S CATALOG NO		
FHWA-CA-TL-78-17				
4. TITLE AND SUBTITLE		5. REPORT DATE		
DYNAMIC MEASUREMENTS OF COMMERCIAL HIGHWAY VEHICLES (WEIGHING-IN-MOTION)		June 1978		
		6. PERFORMING ORGANIZATION CODE		
er de la serie de la companya de la				
	L. Donner, C. E. Frazier	8. PERFORMING ORGANIZATION REPORT 19103-631594		
R. Johnson				
9. PERFORMING ORGANIZATION NAME AND		10. WORK UNIT NO		
Office of Transportation Laboratory California Department of Transportation Sacramento, California 95819		11. CONTRACT OR GRANT NO.		
		C-1-15		
12. SPONSORING AGENCY NAME AND ADDRESS		13. TYPE OF REPORT & PERIOD COVERE		
California Department of Transportation		Final		
Sacramento, California		14. SPONSORING AGENCY CODE		
15. SUPPLEMENTARY NOTES		hall S. Danantmant of		
This study was conduct	ed in cooperation with t I Highway Administration	ne u.s. Department of		
i transportation, redera	The first way Administration	•		
16. ABSTRACT		tall or enoughional		
The research objective	s were to design and ins ing system to screen out	vehicles with probabl		
weight violations and	direct them to a static	platform scale to be		
I stop-weighed and cited	l if in violation of Cali	fornia statutes. Othe		
l vehicles would use a b	ovpass lane where they co	uld be observed for		
potential safety hazards or other violations before allowing non- violators to return to the freeway without stopping.				
Violators to return to	the freeway without see	pp:::9:		
Six pairs of electroni	ic scale weigh bridges we	re installed in a		
l special off-ramp on Interstate 80 at Cordelia, California. A nign				
speed, minicomputer based data acquisition and control system collected data from the scales, determined the axle weight, gross				
weight, axle spacing, and speed.				
}	*			
Typical gross weight	errors were two to three	percent of static		
weight as measured at	the platform scale. Occ The feabibility of weig	ds lonally errors hind-in-motion on an		
I nnorational hacic was	verified. Further study	'is needed to provide		
a more reliable weigh	bridge and to improve th	e Data Acquisition		
I and Control System ope	eration. New state-or-tr	ie-art systems and		
components should be	evaluated with the object	tom		
the dest reatures into	o a fully operational sys	, com e		
17. KEY WORDS	18, DISTRIBUTION ST			
Dynamic weighing, high	h speed No restricti	ons. This document is		
weighing, weighting-intruck scales.	n-motion, available in the Nation:	to the public through al Technical Informatio		
Liuck scales.	Service, Si	ringfield, VA 22161.		
19. SECURITY CLASSIF, LOF THIS REPORTS		21. NO. OF PAGES 22. PRICE		
Unclassified	Unclassified	74		

DS-TL-1242 (Rev.6/76)



# STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION DIVISION OF CONSTRUCTION OFFICE OF TRANSPORTATION LABORATORY

June 1978

FHWA No. C-1-15 TL No. 631594

Mr. C. E. Forbes Chief Engineer

Dear Sir:

I have approved and now submit for your information this final research project report titled:

## DYNAMIC MEASUREMENTS OF COMMERCIAL HIGHWAY VEHICLES (WEIGHING-IN-MOTION)

Study made by General Services Bra	anch
Under the Supervision of Wallace H. Ames, P.	Ε.
Principal Investigator Robert L. Donner, P	.Е.
Co-Investigator Lawrence E. Welsh,	P.E.
Report Prepared by Lawrence E. Welsh, Robert E. Donner, P Charles Frazier	

Very traly yours,

GEORGE A. HILL

Chief of Transportation Laboratory

Attachment

LEW: 1b

#### **ACKNOWLEDGEMENTS**

Many people from various organizations have made significant contributions to this project. The personnel at the Fairfield Maintenance station, under the supervision of Ralph Buss, were extremely helpful with their ideas and manpower.

The California Highway Patrol (CHP) has cooperated fully with us in our efforts. Among those offering assistance were Captain Edward Kynaston, Lieutenant Charles King, Sergeant Loren Zeiss of Headquarters Enforcement Services Division, Commercial Vehicles Section in Sacramento and Captain Bruce Emery and Sergeant Gordon Muir of the field office in Vallejo.

At the Transportation Laboratory, the Machine Shop under the supervision of Floyd Martin and then Joe Wilson helped us many times in our efforts to make the weighing project operational.

Those working directly on the project at various stages included Leonard Alsop, James Butts and Richard Johnson. The programming of the computer for the high speed data acquisition system and also for the data reduction was accomplished by Charles Frazier.

To all the many others who aided us in this project that have not been mentioned, a very sincere "Thank you".

# TABLE OF CONTENTS

	<u>Page</u>
INT RODUCT I ON	1
CONCLUSIONS AND RECOMMENDATIONS	3
FURTHER RECOMMENDED DEVELOPMENT	5
DYNAMIC WEIGHING TEST CONFIGURATION AND OPERATION	8
EQUIPMENT	10
CONTROL & EVALUATION SOFTWARE	13
TECHNICAL DISCUSSION	19
ANALYSIS OF DATA	25
REFERENCES	30
FIGURES	31
ADDENDT V	48

#### INTRODUCTION

Since the State of California Department of Highway Patrol (CHP) first commenced enforcing vehicle weight laws, the primary method of detecting overweight vehicles has been to stop and weigh them on platform scales. The current method used is as follows:

The truck is directed from the freeway by a manually operated or electronic changeable message sign to a weigh station on a special off-ramp. The vehicle is directed to come to a complete stop, then proceed across a 10 ft by 12 ft (3.05 m x 3.66 m) platform scale at a maximum speed of 3 mph (4.38 kmh). The CHP weighmaster then reads the individual axle weights as the vehicle proceeds across the scales. He records the weights, rounded to the nearest 100 lbs (45.4 kg), on an adding machine to obtain the gross vehicle weight. If the truck exceeds a predetermined weight, based on distance between first and last axle, a citation is issued by a CHP officer and the overload must be corrected before the truck is allowed to continue. Citations are also issued if an individual axle exceeds 20,000 lbs (9072 kg), if a group of axles exceeds predetermined weights based on the distance between the axles or if the gross weight exceeds a predetermined weight based on the wheelbase length of the vehicle.

The above procedure is time consuming causing queues of trucks to back up into the freeway lanes. This is a safety hazard to truckers and motorists alike. In addition if a violation is suspected, the truck driver must circle around the scales and come in again for a "stop-weight" check of the violating axle or axles. This "stop-weight" procedure is even more time consuming, causing a more severe safety hazard.

To reduce the safety hazard, the message on the directive signs have generally been changed to direct only loaded trucks to come

to the scales. This allows some relief to the scales, but also allows loaded trucks the opportunity to slip by. At times the sign must be changed to indicate the scales are closed to allow the queue of trucks to be reduced to a safe number for the allowable lane storage available. This temporarily allows all trucks to go by the scales without either being weighed or visually observed for safety violation of the vehicles.

In an effort to improve efficiency of vehicle weight enforcement as well as safety and efficiency of highway operation, and to minimize delay and inconvenience to the trucking industry the California Transportation Laboratory in cooperation with the Federal Highway Administration, designed and placed into operation an experimental "high-speed" truck screening operation. This installation which was located on westbound Interstate 80 at the Cordelia weighing facility, about 45 miles (72.4 km) west of Sacramento, utilized strain gage load cell weighing bridges in a system capable of weighing trucks at speeds up to 35 mph (56.3 kmh).

As the trucks passed over the high-speed scales, the axle weight, axle spacing, speed and gross weight were determined. The weight, and axle spacing were compared with the California load laws to determine if the vehicle is a possible violator. Suspected violators were directed to the platform scales to be weighted statically. Other trucks were directed to a "bypass" lane next to the scale lane where they were observed to determine if their safety inspection sticker was current or if they had some obvious safety hazard. If they were observed to have an outdated inspection sticker or a safety hazard existed, they could be stopped by a signal light and directed by a loud speaker system to drive into an inspection area to be further examined. However, if the

sticker was current and there were no obvious safety deficiencies, they were allowed to proceed in the by pass lane without stopping and to return to the freeway with a minimum of lost time.

#### CONCLUSIONS AND RECOMMENDATIONS

- 1. The practicality of weighing-in-motion on a day-to-day operational basis has been proven. At our particular site, there are geometric problems to be overcome. The weighmaster could not always see the vehicle which was being detected as a possible violator, as the weighmaster is located 800 feet (243.8 m) downstream from the high speed scales location. A closed circuit television (CCTV) installation could be used to solve this problem.
- 2. Typical results show an error in gross vehicle weights approximately two to three percent of the static weight obtained at the platform scales with some gross weight errors exceeding ten percent. Individual axle weights observed varied as much as forty percent of the static weight as measured at the platform scales. This was probably due to the roughness of the pavement leading to the scales and immediately surrounding the scales. This could have been improved by further grinding of the PCC pavement and possibly applying an epoxy overlay. The extremely large axle weight errors did not always contribute to large gross weight errors, apparently due to the purposely designed nonuniform scale spacing and to the sampling method included in the computer program which uses the least deviation from the mean of four successive samples to determine the force a wheel exerts on a scale. This force is then averaged over all six scales.
- 3. Additional work will be required to improve the reliability of some of the electronic equipment. In the early stages of our

project the high speed scanner (multiplexer) - analog-to-digital converter was a continual problem. We eventually re-designed some of the circuitry and improved on its operation. More reliable equipment is now on the market and this should be used in any future installations.

4. It is recommended that further developmental work be done to provide more reliable operational weighing transducers. The strain-gage load cell weighbridges installed at Cordelia proved to be less than satisfactory. We suffered a failure rate of over fifty percent in the transducer itself. Continual efforts to maintain the load plates level with the pavement to eliminate "rocking" or "hammering" on the load cell were unsuccessful. Our machine shop made several modifications in an effort to minimize the excessive maintenance work required. Some success was achieved by milling out the surrounding metal and adding a locknut to reduce movement of the leveling screw. A modified 3-point load plate is now available from the manufacturer (1) which, it is claimed, will eliminate the leveling or "rocking" and "hammering" problem.

Recent literature has shown a scale with the load cell in tension which the manufacturers (2) claim eliminates the problems encountered in our installation at Cordelia. These newer scales should be examined for applicability to high speed weighing.

In review, we recommend a continuation of the effort to bring the system concept proven at Cordelia to full operational status. The anticipated additional work necessary to accomplish this is detailed in the "Further Recommended Development" statement.

<sup>(1)</sup> Rainhart Co., Austin Texas Model 881/882.

<sup>(2) &</sup>quot;The Development of An Automatic Highway Scale," A. Bergan;
G. Dyck; presented to the Canadian Technical Asphalt Association,
Toronto, Ontario, November 1975.

5. We find in evaluating our data and comparing this data with the results obtained from other organizations involved in high speed weighing that our data compares favorably with the results obtained in the United States and Canada. In general it appears that dynamic systems developed and in use by others are utilized for developing loading history rather than for law enforcement.

#### FURTHER RECOMMENDED DEVELOPMENT

It is recommended that existing equipment and facilities at the Cordelia site be used to test and evaluate new developments in weighing transducers. Our intermittent operation of this experimental system over a 2-year period indicates that the following modifications should improve the reliability and overcome many of the present operational difficulties; and ultimately should result in a practical system that can be used as a standard in weighing stations.

#### Geometric and Design Improvements

The first step to possibly improve the data obtained would be to improve the approach to the scale area by grinding and/or resurfacing to reduce the roughness of the present pavement.

Currently, it is possible for the truck to miss one or more of the scales in the lane. Although this may cause the system to abort that run and direct the truck to the scales, it can occasionally cause a number of internal system difficulties. To overcome this difficulty, it is recommended that guardrail or 3-inch (76.2 mm) pipe railing extending over the outside edge of the scales be installed to guide the trucks through the lane.

The overheight indicators are presently located between the last pair of scales and the directional signals. These indicators should be moved to a location within the scale area preferably spanning the last pair of scales. At this location, positive identification of an overheight truck could be made by the system.

In order to eliminate a major source of confusion to the drivers, either the directional signals should be moved closer to the scales or a programmed signal delay, based on truck speed, should be incorporated into the system. At the present time, the directional signals are set immediately after the truck leaves the scales. If the trucks are in a queue, the directional signal is set for a truck possibly two or three vehicles behind the one viewing the signal.

#### <u>Hardware Changes</u>

A closed circuit television (CCTV) system should be installed to assist the weighmaster in determining which vehicle was in violation. If a queue of five or six vehicles is waiting to be weighed statically, the view to the dynamic scales is blocked and the weighmaster cannot identify the violator.

The overheight indicators have ceased to function and are no longer in use. The estimated cost to repair them is at least \$600 each (\$1,200 total). More reliable solid state units are now available and should be purchased to replace the present vacuum tube units.

It is imperative that some positive means be incorporated to determine the presence or absence of a vehicle in the scale lane. This could be accomplished by the installation of either

a series of magnetometers placed down the center of the scale lane at 6-10 feet (1.8-3.1 m) centers or installation of photocells directed diagonally across the scale lane.

It is recommended that the most promising newly developed dynamic weighing scales be evaluated for potential solution of operational problems which were experienced in the prototype system.

Our search for new equipment would place great emphasis on a scale or scales with maximum resistance to wear, vertical movement, or malfunction due to impact loading. This requirement is necessary as any change in elevation between the pavement and the truck scales magnifies impact to the truck tires and suspension system which increases error and variations in readings. New dynamic scale transducer designs may be developed from combining good features of other systems.

#### Program Modifications

The present computer program (implemented in 1975) does not include the recent statuatory changes to the allowable loads which became effective in 1976. A new algorithm to agree with the revised definitions (shown in Figure 3 of this report) must be developed.

Program modifications to incorporate the geometric and hardware changes recommended above should significantly increase system reliability.

#### Additional Parameter

In addition to weight, axle spacing and height information, other parameters could be measured and recorded at a dynamic weighing

site. Width measurement could be obtained and violations indicated. Width is a much more difficult measurement to make than height but vertical photocell arrays have been designed to accomplish this. Automatic vehicle identification is another input which could be used to determine origin and destination or to determine the expiration of safety inspection. Current methods to identify vehicles include a passive microwave label developed by Fairchild Corp. and used by the U.S. Army and the multi-color optical I.D. System used by the railroad industry.

### DYNAMIC WEIGHTING TEST CONFIGURATION AND OPERATION

This dynamic weighing project was conducted at the Cordelia Weigh Station, operated by the California Highway Patrol, on Interstate Highway 80 about 45 miles (72.4 km) west of Sacramento and 48 miles (77.2 km) east of San Francisco, Calif. as shown in Figure The plan view of the site is shown in Figure 2. This weigh station, as most of the larger stations in California, includes weighing and observing trucks to determine those that are overweight, overwidth, or overheight and inspection to determine vehicular safety equipment deficiencies. The operation of the scales is discussed in the introduction of this report. The purpose of this study was to place dynamic weight measuring equipment in the approach to the static scales in order to screen out the obvious weight violators from the obvious nonviolators and allow the non-violators to proceed without delay on a bypass lane. This would result in less delay to the trucker, shorter queues, and lower workload on the weigh-master at the scales.

As shown in Figure 2, the trucks would be directed to the off-ramp leading to the scales by a changeable message sign. Although the data acquisition equipment would be able to obtain wheel weights

at truck speeds approaching 35 mph (56 Km/h), the off-ramp is posted for a 10 mph (16 Km/h) speed limit. This lower speed across the dynamic scales allows a greater number of wheel load samples to be obtained and also allows the trucker sufficient time to correctly interpret the directional signals to the bypass lane or to the static scales.

Immediately in front of the dynamic scales is an inductive loop vehicle detector to alert the data acquisition equipment of the approaching vehicle. As the vehicle traverses the weighing area, each dynamic scale is sampled at the rate of 200 readings/second. This is equivalent to approximately 14 valid samples/tire/scale assuming a 10 mph (16 Km/h) speed and a tire print of 1 foot (0.3 m). Of the samples obtained from each dynamic scale for a given wheel, the mean of those 4 consecutive samples having the least sum of absolute deviations from its mean is used as the wheel weight obtained for that scale. The axle weight is determined by summing the wheel weights obtained on each scale and dividing by the number of scale pairs (in this case n=6) in the system. speed of the vehicle is determined from the amount of time the first axle takes to traverse the last two scale pairs. The axle spacing is then determined from the time-space relationship of subsequent axles.

With the axle spacing and weight information the computer then proceeds to calculate the combined weight of axle groups and the gross weight of the vehicle. This information is compared with the vehicle code shown in Figure 3. If a violation is detected, the computer changes the directional signal to route the truck to the static scales by displaying a red light on the bypass lane and a green arrow pointing to the static scales. At the static scale house detailed information is stored on digital magnetic tape for future computer analysis. Summary information can be printed on a teletype.

In addition to teletype printouts of all potential violators, or optionally all truck data, the weighmaster is notified of the potential violation through a control box mounted by the scale console. The control box allows him to manually control the directional indicator or to put them under computer control. It also indicates to him by an audible tone that a violation has occurred and by lights what the class violation was, e.g. gross, axle or group of axles. For more detail of the exact weights and which axle, the weighmaster may refer to the teletype printout.

#### EQUIPMENT

The equipment scheme used in this dynamic weighing project is shown in the block diagram in Figure 4. In order of data flow this figure shows the wheel load transducers, the high speed multiplexer, the minicomputer, the directional signals, the weighmasters indicator and control box, the display board, the digital magnetic tape unit, and the teletype printer.

#### Wheel Load Transducer

The wheel load transducer assembly is shown in Figure 5. It consists of a transducer frame which is placed on bearing pads grouted into a scale pit approximately 3-1/4 inches (82.6 mm) deep. The scale frame supports the electronic load cell chassis. The chassis contains eight active and eight temperature compensating strain gage load cells which are wired together in the configuration of a wheatstone bridge as shown in Figure 6. The vehicle load is transmitted to these load cells through three one inch load plates which are placed upon the top of the load cell chassis. All of the electrical connections on the electronic

load cell chassis and to the outside road are made through sealed copper tubing which is pressurized with nitrogen gas which precludes the intrusion of moisture into the electronic system.

The load cells in their wheatstone bridge configuration are excited with a DC power supply of approximately 30 volts, this voltage is adjustable in order to calibrate the individual scales. The output of the scales is approximately 10 millivolts for a full load input of 10 kips. The output of the scale platform is amplified by a DC amplifier and wired to the input of the multiplexer/analog-to-digital converter.

## Multiplexer/Analog-to-Digital Converter

The output signals from the load cells are connected to the twelve inputs of the multiplexer/analog digital converter. This device subsequently scans the transducers at a rate of approximately 10,000 samples per second, amplifies the signal to an acceptable level, then converts the magnitude of the analog signal to a corresponding digital code acceptable for transfer to the computer.

#### Digital Computer

The digital computer used in this system performs four basic functions; collection and reduction of the data presented from the load cells to determine the equivalent static weight of each axle on a vehicle, comparison of these weights with the vehicle code to determine violations, controlling the traffic signals for the vehicle, and providing information to the weighmaster through the control box lights and/or teletype.

#### Directional Signals

Two 2-faced directional signals are placed over the bypass lane and the static scale lane. These signals display either a combination of a green arrow to the bypass lane and a red ball to the static scales or a green arrow to the static scales and a red ball to the bypass lane. These directional signals can be operated under computer control or manually by the weighmaster.

#### Weighmaster Control Box and Display Panel

A control box is placed near the weighmasters static scale console which allows him to control the directional indicators manually or under computer control. This box also contains lights to indicate the type of violation of the truck entering the static scale area. These lights indicate gross violations, axle violations, combination of axle violations, or an abort. An abort indication is signaled to the weighmaster when for some reason the computer is unable to determine the actual weight of the vehicle. This situation can occur when the trucker has changed speed drastically through the scale platform area or has driven in the shoulder area where proper weight determination cannot be made. In these cases, the truck will always be weighed.

#### Digital Magnetic Tape and Teletype Printer

A digital magnetic tape unit is provided to permanently record all dynamic weights from the digital computer. These weight records contain the truck number, the time of day, and each individual wheel weight determination. This information can also be printed on the teletype printer in a format shown in Figure 7. This teletype printer output can be of assistance to the weighmaster to determine the actual type of violation which has occurred.

## CONTROL & EVALUATION SOFTWARE

The computer program for this project was written in assembly language and uses the direct memory access option for output operations to the (teletype) printer and the 9-track digital magnetic tape recorder. Simplified flow charts for the data acquisition section and the data reduction section are attached. Other sections not shown include the site initialization routine, the daily startup routine and the diagnostic routines which provide a histogram of multiplexer readings and continuous output of readings from a selected multiplexer channel.

In describing the operations of the data acquisition and reduction sections of this program, it is necessary to describe certain attributes of the system and nomenclature:

There are an even number, N, of dynamic scales and associated multiplexer channels. All even numbered scales are used to read the loads on one end of each axle and all odd numbered scales are used to read the loads on the opposite end of each axle.

For each scale, there is a value, ZER(I), consisting of the sum of a constant representing the cutoff value below which multiplexer readings are disregarded and a variable representing the most current multiplexer reading at no load.

When the scale is loaded, the multiplexer value is driven negative proportionally to the applied weight. To determine whether to use this value in estimating the applied load, ZER(I) is added to the value. If the resultant is negative, this value becomes MUX(I) during subsequent operations. (The true weight factor is found

by adding the ZER(I) to the absolute value of MUX(I).) If the resultant is positive, the number of immediately prior consecutive negative values for that scale is placed in MUX(I).

When a truck approaches the scales, it is assigned one of eight truck information storage buffers, TISB, which is used to store data for the first 9 axles on that truck. This data includes the truck number, time of day, data for each axle from each scale, timing data to determine axle spacing and speed and violation or abort information. This information is then stored on 9-track magnetic tape for later analysis and evaluation.

For each scale, I, there is a scale buffer containing the following:

- V(I,1) Through (V(I,4) = the latest four MUX(I) obtained in the current weighing cycle.
- PNTR(I) = A pointer to the earliest V(i,j) obtained (to be replaced by the next MUX(I) in current cycle)
- SUM(I) = The current sum of (V(I,1) through V(I,4).
- LAD(I) = The lowest sum of absolute deviations of V(i,j) from the mean, SUM(I), found in the current cycle.
- ADDR(I) = An address in TISB for storage of the mean having a minimum value of LAD(I).
- AFLG(I) = First axle indicator and axle counter.
- SCNTS(I) = Number of consecutive negative MUX(I) obtained.

## Program Operation

Operations occur in two distinct areas or program sections.

Primarily, the program operates in the data reduction and output section, EXEC, to be described later. Every 5 milliseconds, current operations are suspended or interrupted and control is given to the data acquisition and evaluation section.

# Data Acquisition and Evaluation

STEP 1 - Data Acquisition

A multiplexer reading is obtained for each scale at 100  $\mu \text{sec.}$  intervals.

- a. If no truck is in the scale area the readings obtained are used to update each modified scale zero value, ZER(I). Go to step 3.
- b. If a truck is in the scale area, MUX(I) = multiplexer value + ZER(I) is calculated.
  - 1. If MUX(I) is positive (indicating an invalid reading), the value in SCNTS(I) is placed in MUX(I). SCNTS(I) and V(I,1) to V(I,4) are set to zero.
  - 2. If MUX(I) is negative, both SUM(I) and PNTR(I) are updated.

# STEP 2 - Data Evaluation - for each MUX(I)

- replace V(I,PNTR(I)) with MUX(I) if SCNTS(I) is greater than 3
  - l. Calcualte the sum of absolute deviations from SUM(I)/4 for the V(i,j).
    - 2. If the resultant is less than LAD(I), store resultant in LAD(I) and store SUM(I)/4 in TISB at ADDR(I).
- b. If MUX(I) = 0, no action.
- vector for the next wheel.
- 1. If scale (N) or (N-2), store time interval in TISB for determination of axle spacing.
  - 2. If scale (N) or (N-1), check for abnormal operation and set proper flag in TISB as axle leaves that scale.
  - 3. If not scale (N) or scale (N-1) and first axle is leaving, initialize ADDR(I) and AFLG(I) for the next scale in series. (Scale I+2)

#### STEP 3 - Update Truck Counters

- a. If manual reset is on and all output operations are complete, set 'on' and 'off' truck counts equal to the 'output' truck count. Then go to step 4.
- b. If the 'off' loop detecter has changed from 'on' state to 'off' state, increment 'off' truck count.
- c. If the 'on' loop detector has changed from 'off' state to 'on' state:
  - 1. Increment 'on' truck count.
  - 2. Assign, in order, one of eight TISB's to the oncoming truck. Store truck number and time of day in the assigned TISB.
  - 3. Store proper TISB addresses in ADDR(1) and ADDR(2), initialize AFLG(1) and AFLG(2).

STEP 4 - Update Time of Day

STEP 5 - Return to Suspended Operation

## Data Reduction and Output

Program 'EXEC' is primarily used to direct control to the data reduction routine when data for each truck axle is complete and to initiate output operations to the printer and/or 9-track magnetic tape at the proper time. While cycling, it also checks the overheight indicators and a manually set end of day indicator.

As indicated on the attached flow chart (Figure 9), printed output occurs each time the data for an axle has been reduced. After data for the last axle has been printed and TISB for that truck is written onto magnetic tape and then the gross weight, distance from first to last axle and any violations or abort indications are printed. 'EXEC' cycles through this sequence until directed to the end of day routine which, after a clean-up procedure, halts all operations.

#### TECHNICAL DISCUSSION

The high speed scale layout is located approximately 800 ft (243.8 m) upstream from a 10 ft by 12 ft (3.05 m by 3.66 m) platform scale, static weighing station at Cordelia in a specially modified off-ramp from the freeway. The portland cement concrete paved lane containing the weigh-in-motion scales is built to State of California Standard Specifications except with the addition of No. 6 reinforcing bars longitudinally at 6 in. (152.4 mm) centers located at depth of 5 ins. (127 mm) and No. 4 bars transversely at 18 in. (4.57 m) centers. The bars extend to within 1 1/2 ins. (38.1 mm) of the joints. Reinforcement was added to minimize variations in pavement profile due to thermal and moisture variations and thereby to minimize dynamic effects on wheel and axle loads as they pass across the weigh-in-motion scales. A parallel or by-pass lane is provided to allow maintenance of the scales. Maximum truck volume is approximately 2,100 vehicles per day in August decreasing to 1,100 vehicles per day in December.

The scales are located with an increasing longitudinal distance between units as shown in Figure 8. This spacing was designed to minimize the probability that the vibration frequency (or some harmonic) of the truck suspension or tires would correspond to the distance between transducers at some responsive speed. The spacing between the first and last transducer assembly layout is approximately 44 ft (13.4 m).

The scale frames, which are still in place, are installed in a high strength epoxy adhesive to preclude their working loose. The electronic strain gage, load cell scales, manufactured by Rainhart Company of Austin, Texas, are approximately 22 ins.

by 49 ins. (.56 m by 1.24 m). The scales were installed in pairs so that the wheels on opposite ends of an axle were weighed individually, but at the same time. There were six pairs of scales in the installation, with provision for a seventh pair. Dry nitrogen was supplied directly to each electronic chassis from a manifold with individual pressure regulators for each chassis. The nitrogen tank was replaced with a full tank about once a month during the system operation.

The truck screening project was in operation intermittently between November of 1974 and early 1977. A statistical experiment was designed and performed in May of 1975 with a loaded five axle truck. Unfortunately a scale failed during the test and the results were not meaningful. Six of the scales had failed during the period between November 1974 and June 1975. These were returned to the manufacturer for repair (as they failed) and were re-installed upon their return from the manufacturer.

In August of 1975, (due to administrative action outside the control of the project) the operation was shut down and all the electronic gear moved from the office trailer near the dynamic scales into the weighmaster's scale house. This involved digging trenches, placing the signal power and loop detector wiring inside schedule 80 PVC pipe and burying them 18" below grade in a sand bed. This move added an additional 600 feet of wire in the signal circuits with the attendant shielding and noise problems. We were not able to return to operation until the end of December 1975.

During early 1976 we worked at resolving the various problems we had faced before. Different methods were tested to reduce the hammering and rocking of the load plates. Our machine

shop put in many hours working on the various ideas put forth in the hopes of eliminating the problem. Improvements were made but these actions did not solve the problem that we feel is due to the basic load plate assembly design.

In March of 1976 we began a series of tests to determine the overall system reliability and accuracy. The scales and system were recalibrated by the local (Solano County) Weights and Measures Authority. During this testing period we experienced computer program problems as we could not correlate the magnetic tape truck number and data with the paper tape (Teletype) truck number and data. As we had developed several computer programs to analyze the magnetic tape data, we were forced to halt the tests until we could resolve the truck count error problem. A partial solution was reached whereby we could reset the truck number to keep the program running correctly.

A new series of tests were run during June of 1976 which we feel proved feasibility of the system concept. The data from those tests with our analysis is shown in the Appendix.

#### Loop Detectors

Two loops are used in the pavement, with their associated loop amplifiers, to determine if there is a truck in the scale area. One loop is 6 ft (1.83 m) upstream from the first pair of scales; the second loop is 6 ft (1.83 m) after the last pair of scales. The trucks are counted in and out by the computer program.

#### Height Indicators

Two standard photo-electric height indicators are located approximately 22 ft (6.7 m) after the last pair of scales. One indicator is 13.5 ft (4.1 m); the other is 14.0 ft (4.27 m)

above ground in accordance with the State of California Vehicle Code. An audible alarm alerts the weighmaster at the static scale when a vehicle exceeds either height limit. As mentioned before this system failed but can be easily upgraded to a reliable system through the use of off-the-shelf equipment at a nominal cost.

#### Electronic Equipment

The data acquisition and control system used to obtain wheel weight, axle spacing and speed consists of the following units:

- 1. 12 Strain Gage Power Supplies.
- 2. Multiplexer/Analog to Digital converter.
- 3. 16 Bit Minicomputer with 4K of Core Memory, Real Time Clock, Direct Memory Access, and 32 Bits of Digital Input/Output.
- 4. Teletype.
- 5. 9-Track, 800 bpi. Digital Magnetic Tape Recorder.
- 6. Violation Indication Display.

#### Overall Description of Truck Screening Installation

Twelve separate strain gage power supplies furnish power to the electronic scale chassis. This allows each scale to be calibrated very easily. The force exerted by the tire on the transducer assembly produces an output signal voltage proportional to that force with each 10,000 lbs (4,536 kg) increment of force producing a ten millivolt signal. The excitation voltage and the output

signal voltage are brought to each transducer in 0.5 in. (1.27 cm) diameter copper tubing which also supplies a protective envelope of dry nitrogen gas at a slight positive pressure of 2 psi (1.406 kgs/ $m^2$ ). The nitrogen gas is used to impede moisture from entering the strain gage load cells.

The output signal voltage (proportional to the vertical force) is connected to the Multiplexer/Analog to Digital converter. This device sequentially scans the transducers at a rate of 13,900 samples per second, amplifies the signal to an acceptable level, then converts the magnitude of the D.C. signal to a corresponding binary code acceptable for transfer to the computer.

In the computer the vertical forces exerted by the wheel on the transducer assembly are averaged over the four successive samples above a pre-selected cutoff value which have the least deviation from their mean. This average force is then added to the average force obtained for the wheel on the other five scales as that wheel goes over each scale. This sum is then divided by six to obtain an overall average weight for that wheel. This average force is added to the average force obtained for the wheel on the other end of the axle to obtain an average axle weight. This process is repeated for each axle of the vehicle as it crosses each of the six pairs of transducers.

The computer program, written in Assembly language, is contained in 3,500 words of the available 4,096 words.

During the time the truck is being dynamically weighed, the space between axles is also determined to the nearest 1 ft (.305 m). Knowing the axle weight and spacing, the truck can then be compared with the load laws as set forth in the Vehicle Code. If a violation is detected, the system prints the type of violation on the

teletype and by means of overhead signals, directs the truck to the platform scales to be re-weighed "statically" by the weighmaster. If the truck is determined to be in violation of the load laws, the driver is cited and must correct the violation before he can move the vehicle from the weighing station. Vehicle speed is also calculated and if a change in speed of more than 25% is detected, an "abort" situation is declared. The vehicle is then directed to the platform scales to be weighed.

If the vehicle is not in violation and does not "abort", it is directed by means of the overhead signals to a by-pass or "hot" Tane to allow it to return to the freeway without being stopped at the platform scales.

Violations are indicated to the weighmaster by a small display mounted in front of him. The weighmaster has control of the overhead signals and can direct all vehicles to come to the platform scale if he so wishes. This is to allow the weighmaster to determine if the truck needs a mechanical inspection, or to see if it has some obvious safety deficiency.

#### ANALYSIS OF DATA

#### Conclusions

- 1. The use of a dynamic weighing system as described in this report can be used effectively in reducing the number of vehicles that need to be weighed on static scales to determine compliance with vehicle code requirements. Based on a "typical" day where 2148 vehicles entered the scale area, approximately 20% would be directed to the static scales as 'possible violation' and approximately 6% would be 'aborted'. Some of these 'aborted' vehicles were light-duty vehicles and would not be weighed.
- 2. Significant differences were obtained in the precision of weighing between scale pair combinations. Because of the method used in collecting data for analysis, the reason for these differences, (distance between scale pairs, scale characteristics or other factors) could not be determined. Using the present dynamic scales, it is felt that adequate screening of vehicles can be accomplished using the 4 scale pair combination listed in the following table.

Based on least-square linear regression analyses and using a 99% confidence level, the following table lists those scale combinations found to be most effective in determining axle loads:

No. of	Scale Pair	% Variance of	Actual Load (.99 CL) Tandem Axles*
Scale Pairs	Nos.	Single Axles	
6	A11	15.3	8.2
5	2,3,4,5&6	15.2	8.0
4**	2,3,4&6	16.1	8.0
3	2,4&6	17.4	8.6
2	2&6	19.8	9.2

<sup>\*</sup>Based on 34-Kip axle loading.
\*\*Recommended scale-pair combination.

3. It is imperative that means be taken to insure that the full wheel load is impressed on each dynamic scale as the vehicle traverses the scale area. Allowing one wheel to come only in partial contact with the dynamic scale not only could allow an overweight vehicle to bypass the static scales, but also has caused errors in minicomputer data storage routines.

#### Data Collection

To determine the accuracy of axle weights obtained using the dynamic scales, 'stop weights' were obtained on each single axle and pair of tandem axles on 162 trucks selected at random from those statically weighed on March 25 and June 15, 1976. These 'stop weights' were obtained by having the truck move over the platform scales until a single axle or pair of tandem axles was isolated on the weighing platform. The driver was then requested to release the vehicle's brakes to relieve platform friction and the weight was recorded to the nearest 100 pounds (45.4 kg). This 'stop weight' data was then used with the dynamic scale data obtained for that truck in these analyses. In this manner, data for 435 single axles and 175 tandem axles was collected over the two days.

#### Data Preparation

Because stop weights were not obtained on individual axles of tandem axle groups (less than 5 feet (1.52 m) between axles), the dynamic scale data for the two axles were combined for comparison with the static weights. The data was then screened to eliminate those outliers which could be identified as either geometric design deficiencies and/or operational problems. The remaining data was separated into two groups; one containing data on 429 single axles and the other containing data on 171 tandem axles.

31

#### Analysis of Data

Step 1 The first step of analysis consisted of performing least-squares regression analyses using the mean of all dynamic scale-pair readings as the response variable and the residual of dynamic minus static scale readings as the dependent variable for each group as shown in Figure Al for the single axle group and Figure A2 for the tandem axle group. Inspection of these results indicated that, although this analysis was adequate for the tandem axle group, the variances for the single axle group appeared to be proportional to the dynamic scale reading. Dividing the residual by the static weight and using this result as the dependent variable for the single axle group provided the regression shown in Figure A3 Although this may have caused slight overcompensation for the variances, it was considered suitable for this analysis.

This step in the analyses resulted in determining the following generalized equations to be used in subsequent steps:

For single axle determinations:

 $(D-S)/S = B\emptyset + B1 * D$ 

For tandem axle determinations:

 $D-S = B\emptyset + B1 * D$ 

Where

BØ = Intercept value

B1 = Slope

D = Weight from dynamic scale-pairs

S = Static stop weight.

Step 2 This step consisted of performing regression analyses on each combination of dynamic scale-pairs using from 2 to 6 pairs of dynamic scales. In addition to obtaining regression

coefficients and other parameters required for further analysis, 'critical values' were calculated for designated significance levels in each analysis. The 'critical value' for a designated significance level is that dynamic scale value having the significance level probability of 20 Kip single (or 34 Kip tandem) static weight. This critical value is the dynamic scale value above which vehicles should be directed to the static weighing scales.

Following the table of critical values are tables showing the actual number of axles above and below vehicle code requirements, the number of axles which would 'pass' or must 'stop' for static weighing and the 'calculated' or normal curve probabilities for these occurrances. In all of these analyses, the calculated violations were higher than the actual violations for both single and tandem axles indicating the degree of nonconformity to a normal probability distribution resulting from previous assumptions made in this analysis and departure from normally distributed axle weights in the data. These differences were minimal for the recommended scale-pair combinations.

Step 3 This stop consisted of a 'dummy run' of the 162 vehicles for which 'stop weight' data was collected including those vehicles where data contained outliers which were not used in steps 1 and 2. Using the regression parameters obtained in step 2, tables of actual and calculated operational values were calculated for each of 5 significance levels. Only single axle and tandem axle violations were considered in this Step and in Step 4.

Step 4 This step consisted of simulating the results from a 'typical' day. Based on the data stored on magnetic tape by the system on June 15, 1976 and using various dynamic scalepairs, the same procedure as was used in step 3 was used to develop information concerning the effectiveness of the dynamic

scales. It should be noted that the number of calculated violations are exceptionally high when compared to the 8 actual violations that occurred.

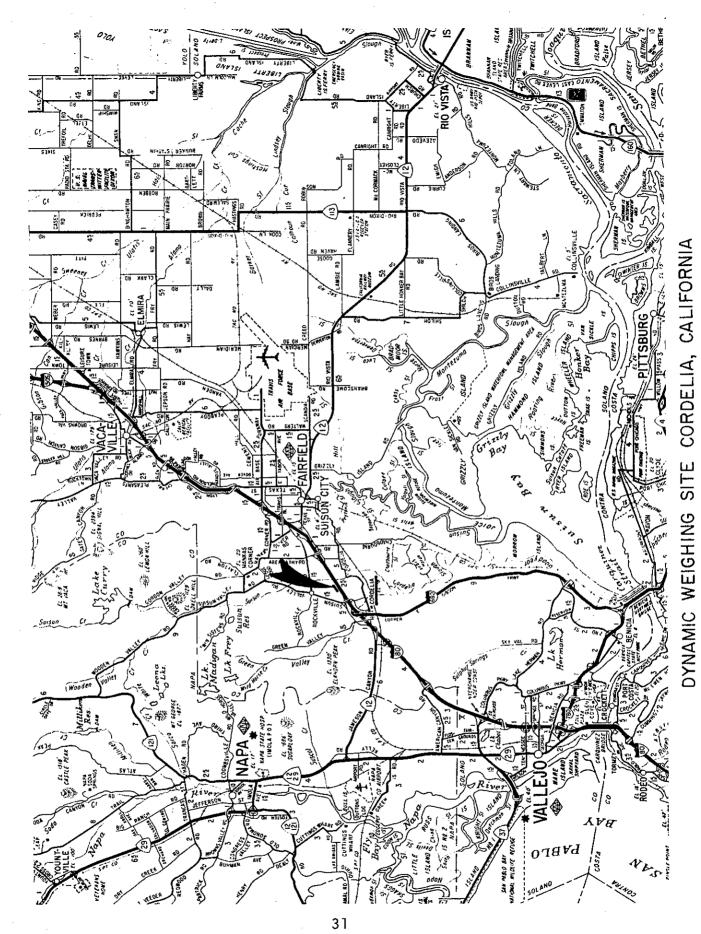
Two sources which probably were the major cause of this discrepancy were:

- a. The actual legal load limits of 20 Kips on single axles and 34 Kips on tandem axles was used in this analysis. In actual practice, however, tolerances of up to 5% are allowed on the static weights before the load is considered to be in violation.
- b. It was noted particularly in Figure A3 that the distribution of axles by load was a bimodal distribution, and the distribution of residuals in the 15 to 20 Kip range were negatively skewed. This analysis was based on a normal curve distribution and no correction was made to correct for this skew.

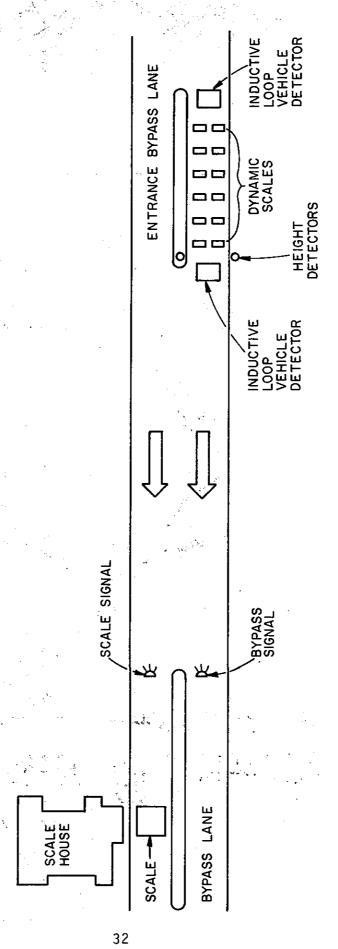
It appears that, using the four dynamic scale-pairs recommended in this section, approximately 50 percent of the 1068 vehicles actually weighed on this 'typical' day would have been allowed to bypass static weighing with negligible probability of having a weight violation. This assumption is based on the type of each violation recorded for this 'Typical' day and the proportion of vehicles stopped for static weighing to the number of vehicles found in violation of the vehicle weight code.

#### REFERENCES

- Department of Civil Engineering, University of Kentucky, "Weighing Vehicles in Motion," HPS-HPR-1(25), April 1964.
- 2. Herrick, R. C., "Analytical Study of Weighing Methods for Highway Vehicles on Motion," HRB, HR7-3, July 1967.
- 3. Lee, C. E., and AT-Rashid, N. II, "A Portable Electronic Scale for Weighing Vehicles in Motion," Report 54-IF, Center for Highway Research, University of Texas at Austin, April 1968.
- 4. Machemehl, R. B., Lee, C. E., and Walton, C. M., "Truck Weight Surveys By In-Motion Weighing," FHWA Project 3-10-74-181, September 1975.
- 5. McCann, H., Dean, E., and Boale, R., "The Texas Procedure for Weighing Trucks in Motion," DOT, FHWA, Highway Technical Report #36, May 1974.
- 6. Burgess, J. P., and Smith, R. A., "Evaluation of Dynamic Vehicle Weighing System," Paper Presented I.T.E. Conference, Halifax N.S., April 1975.



N FIGURE



PLAN VIEW OF DYNAMIC WEIGHING SITE

## CHAPTER 5. WEIGHT

Article 1. Axle Limits

# Maximum Weight on Single Axle or Wheels

35550. (a) The gross weight imposed upon the highway by the wheels on any one axle of a vehicle shall not exceed 20,000 pounds and the gross weight upon any one wheel, or wheels, supporting one end of an axle, and resting upon the roadway, shall not exceed 10.500 pounds, except that the gross weight imposed upon the highway by the wheels on any front steering axle of a motor vehicle shall not exceed 12,500 pounds.

(b) The gross weight limit provided for weight bearing upon any one wheel, or wheels, supporting one end of an axle shall not apply to vehicles the loads of which consist of livestock

(c) The following vehicles are exempt from the front axle weight limits

specified in this section:

rucks transporting vehicles.

Trucks transporting livestock.

Dump trucks. Cranes.

(5) Buses. (6) Transit mix concrete or cement trucks, and trucks that mix concrete or cement at, or adjacent to, a jobsite

Motor vehicles that are not commercial vehicles.

Vehicles operated by any public utility furnishing electricity, gas, water, or telephone service.

(9) Trucks or truck tractors with a front axle at least four feet to the rear of the foremost part of the truck or truck tractor, not including the front bumper.

0) Trucks transporting garbage, rubbish, or refuse.
1) Trucks equipped with a fifth wheel when towing a semitrailer.

(12) Tank trucks which have a cargo capacity of at least 1,500 gallons. Amended Ch. 268, Stats. 1939. Effective Sept. 18, 1939.
Amended Ch. 631, Stats. 1970. Effective Nov. 23, 1970.
Amended Ch. 169, Stats. 1971. Operative May 3, 1972.
Amended Ch. 631, Stats. 1975. Effective January 1, 1976. Superseding Ch. 132.
Amended Ch. 48, Stats. 1976. Effective March 17, 1976, by terms of an urgency clause.

## Computation of Allowable Gross Weight

(a) ( ) Except as otherwise provided in this section or Section 33551.5, the total gross weight in pounds imposed on the highway by any group of two or more consecutive axles shall not exceed that given for the respective distance in the following table:

between the extremes of any group of 2 or Distance in feet

more consecutive

axies	2 axles	3 axles	4 axloc	J.
*************************************	34,000	34.000	34.000	, .
		34,000	34,000	יו ניי,
······································		34,000	34,000	) C.
7		34,000	34,000	, (7)
		34,000	34,000	יים ו
B	30,00	49 ≒00	000	, ,

U	200	3	04.000	2
	34,000	34,000	34.000	200
Ç	200		200	3
7		30,5	34,000	34,000
α	34,000	34,000	34,000	34,000
	34,000	34,000	34,000	34,000
10	39.000 39.000	42,500	42,500	42,500
11	40,000	43,500	43,500	50.5
10	40,000	44,000	44,000	200
1.0	40,000	45,000	50,000	0000
1.0	40,000 +0,000	45,500	50,500	00.00
The state of the s	000,000	16.500	51,500	51.500
18	000 000 000 000 000 000 000 000 000 00	47,000	52,000	52,000
7.7	000,0 <del>1</del>	900°8	52,500	52.500
10	<del>1</del> 0,000	84 500 500 500	53,500	53,500
70	40,000	49,500	54,000	000 75

	<u> </u>	Distance in feet		-				1
-	و ۱			J AXIES	4 axles	5 axles	6 axles	
- c	<u> </u>			20,000	006 16	54,500	54,500	
4 C	3 =			51,000	55,500	55,500	55,500	
1 C	- 9	***************************************		51,500	36,000	56,000	26 000	
ΝĊ	9 5	***************************************		52,500	26,300	26,500	56.500	
4 c	3.2	***************************************		53,000	57,500	57.500	57,500	
V Ĉ	, u	***************************************		54,000	58,000	58,000	000.85	
V Č	9			54,500	58,500	000,83	0000	
٦ ¢	9 1	***************************************		55.500	59,500	59,500	00000	
Νč	- 0	***************************************		56,000	90,000	90.00	00009	
<b>ৰ</b> হ	o c	***************************************		57,000	90000	60500	60.500	
5 K	ה כ			57,500	61,500	61,500	61500	
5 2	> -	***************************************		58,500	62,000	62,000	62,000	
รี่ ถึ	- c			59,000	62,500	62.500	62,500	
วี ถึ	; ) c			900,09	63,500	63.500	63,500	
36	: ? =	***************************************		60,000	64,000	000	64,000	
2 ¢	: * )	***************************************		60,000	64,500	64.500	500	
3 8	: > 4			60,000	65,500	55.50	65.500	
ጓ <u>የ</u>	: :	***************************************		90,000	000:99	96,000	900099	
2 6	:	***************************************		000'09	66,300	96.500	66.500	
36	: n c	***************************************		90,000	67,500	67,500	67.500	
3 5	: :	***************************************		90,000	68,000	68 000	9	
⊋ ₹	:	***************************************		90,000	68,500	70,000	20,07	
7 9	:			. 000,09	69,500	72,000	79,000	
¥ ç	;	***************************************		90,000	70,000	73 280	73.980	
? :		***************************************		000'09	70,500	73 280	73 990	
Į.		***************************************		90,000	71,500	73,980	73.980	
<u> ۲</u>	:	***************************************		000009	72,000	7600		
<b>;</b>	:	***************************************		000,09	72,500	76,500		
40	:_	***************************************		000,09	73,500	77,500	88	
\$ <del>{</del>	!	***************************************		00,00	74,000	78,000	8 8 8 8	
r i	!	401031100000000000000000000000000000000		000'09	74,500	78.500	000	
3	1			000,00	75,500	79,000	8000	
2 %	:	***************************************		000,09	76,000	80,000	0000	
3 6	:	***************************************		9000	76,500	80,000	90,000	
3 17	Í			000,00	77,500	80,000	80,000	
5 17	į	***************************************		0000	78,000	80,000	80,000	
3 8	;	***************************************		0000	78,500	80,000	000	
3 6	1	***************************************		00009	79,500	80,000	80,000	
2 8	ŀ			00,00	80,000	80,000	80,000	
3 6	į	***************************************		9000	000,08	80,000	80,000	
: 3 &	į	,	40,000 80,000	0000	0000	80,000	80,000	
;	;	7		90,000	900,000	80,000	80,000	

of tandem axles may carry a gross weight of 34,000 pounds each if the overall distance between the first and last axles of such consecutive sets of tandem axles (b) In addition to the weights specified in subdivision (a), two consecutive sets is 36 feet or more. The gross weight of each set of tandem axles shall not exceed 34,000 pounds and the gross weight of the two consecutive sets of tandem axles

axles 34,000 34,000 34,000 34,000 42,500 43,500 4,000 50,500 51,500 52,000 52,500 53,500 54,000

34,000

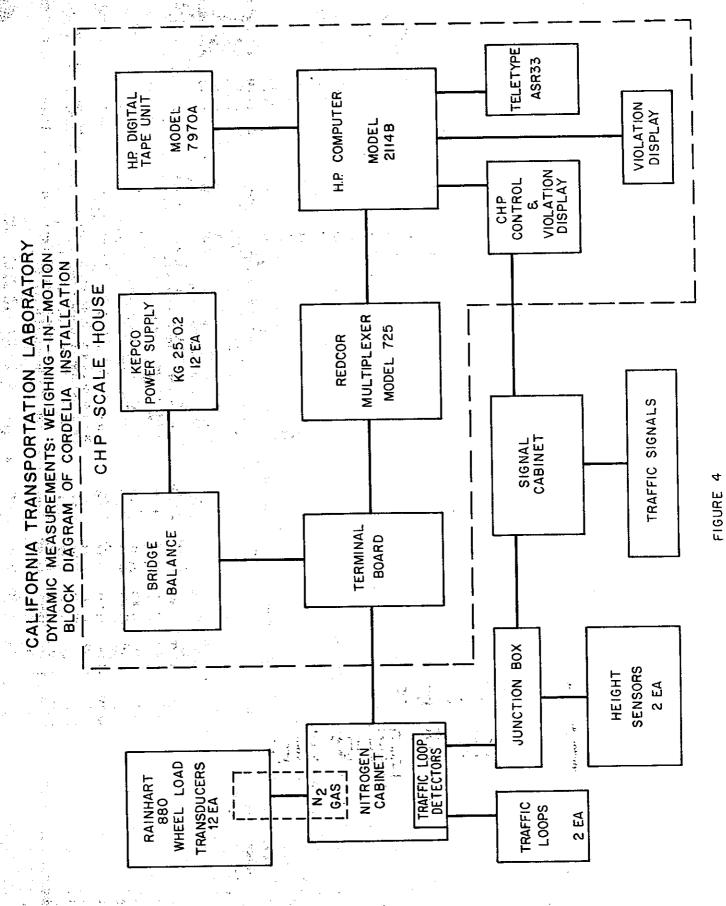
shall not exceed 68,000 pounds.

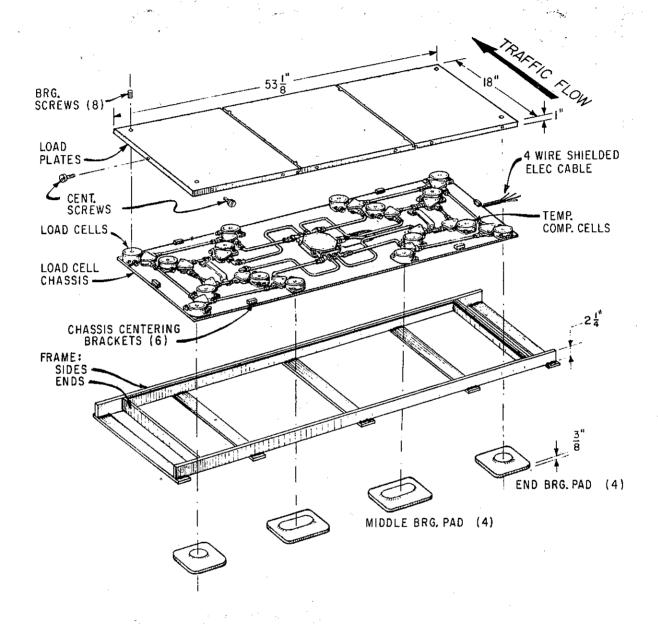
(d) Nothing contained in this section shall affect the right to prohibit the use of any highway or any bridge or other structure thereon in the manner and to the extent specified in Article 4 (commencing with Section 35700) and Article 5 (commencing with Section 35750) of this chapter. (c) The distance between axies shall be measured to the nearest whole foot. When a fraction is exactly six inches, the next larger whole foot shall be used.

(e) The gross weight limits expressed by this section and Section 35550 shall include all enforcement tolerances.

Amended Ch. 1625, Stats. 1961 Effective Sept. 15, 1961.
Amended Ch. 337, Stats. 1965 Effective Sept. 17, 1965.
Amended Ch. 394, Stats. 1970 Effective Nov. 23, 1970.
Repealed and Added Ch. 551, Stats. 1977 Effective January. 1, 1976.
Amended Ch. 166, Stats. 1975 Effective May 11, 1976 by terms of an arconcy clause.

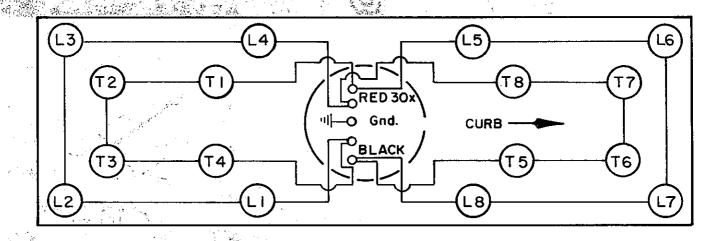
54,000



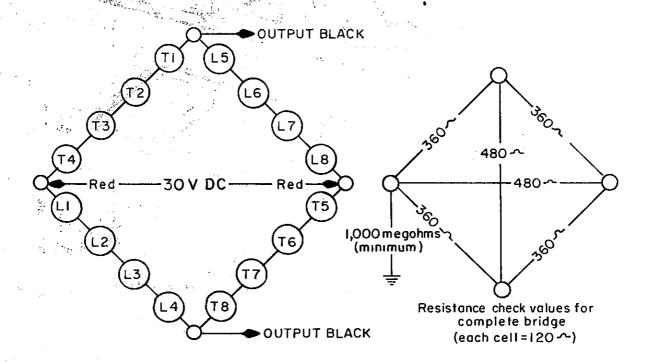


#### WHEEL LOAD TRANSDUCER ASSEMBLY

FIGURE 5



ŧ.



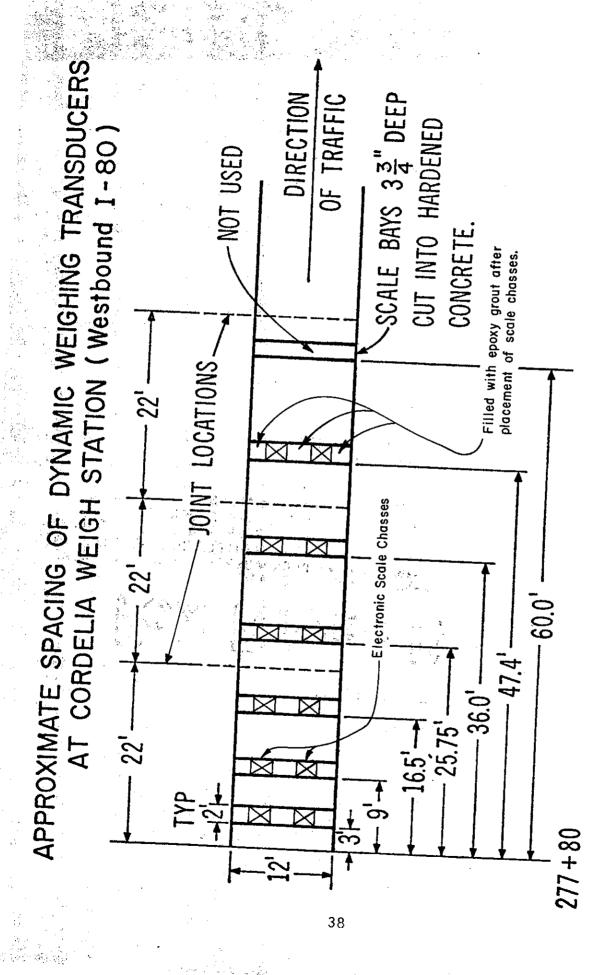
TRANSDUCER (LOAD CELL) CHASSIS SCHEMATIC

Figure 6,

```
TRUCK NUMBER
                #001
                            AXLE SPACING (FEET)
AXLE WEIGHT
                109
   X100#
                   14
                152
                   04
                164
                    29
                 152
                    04
                 163
                              GROSS WEIGHT X100#
                 G = 740
                              TOTAL LENGTH (FEET)
                 L = 051
                              VIOLATION
                 V= NONE
                                               NO VIOLATION
                               (ie) NONE
                                               AXLE 2 VIOLATION
                                    AXLE 2
                                               AXLE GROUP 1 & 2 VIOLATION
                                               TOTAL VEHICLE WEIGHT VIOLATION
                                       2 - 3
                                    GROSS
                                               TRUCK ABORTED COULD NOT READ
                                    ABORT
```

TELETYPE PRINTER OUTPUT

FIGURE 7



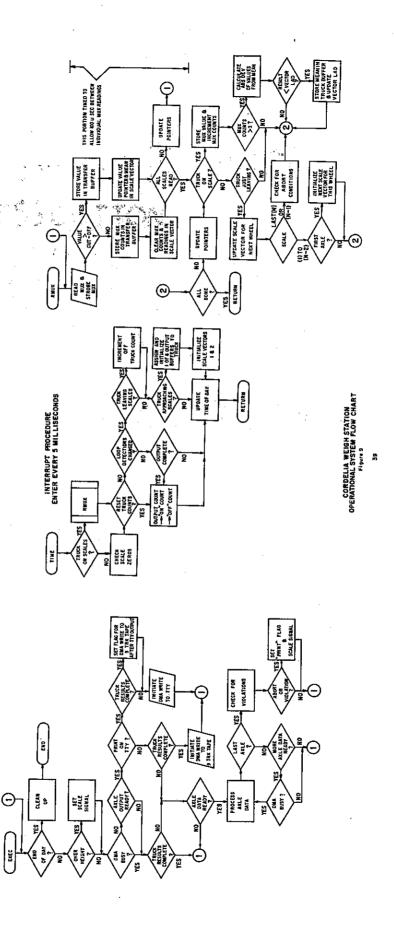
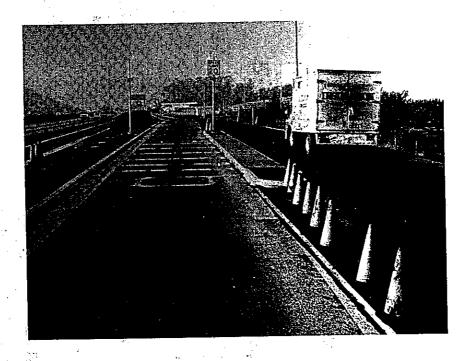
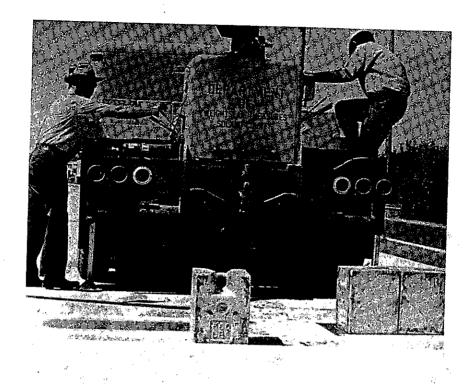


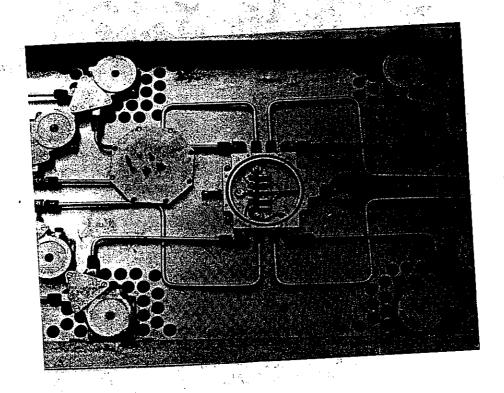
Figure 10



COMPLETE SCALE INSTALLATION WITH DIRECTIONAL SIGNALS AND STATIC SCALE HOUSE IN THE BACKGROUND

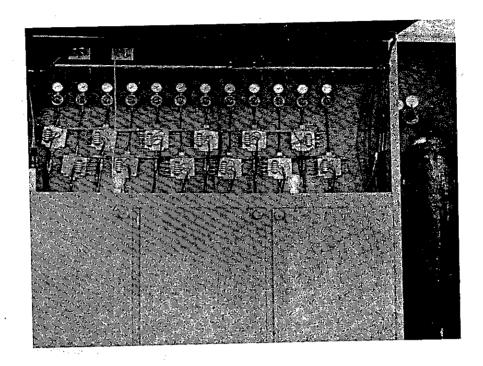


STATIC CALIBRATION OF DYNAMIC SCALES



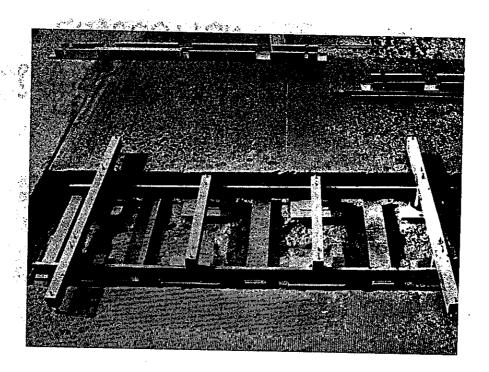
STRAIN GAGE LOAD CELL PLATE WITH SEALED ELECTRICAL CONNECTIONS IN THE CENTER. NOTE TUBING TO EACH CELL FOR NITROGEN MOISTURE SYSTEM

Figure 13



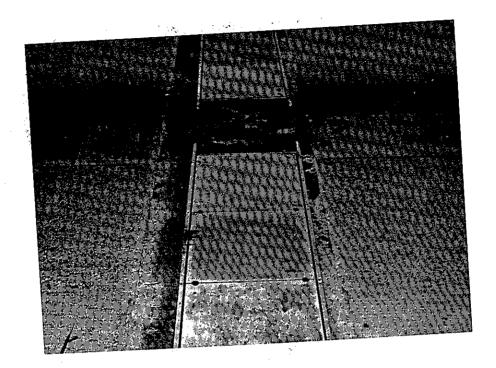
MAIN NITROGEN MANIFOLD FEEDING EACH SCALE

#### Figure 14

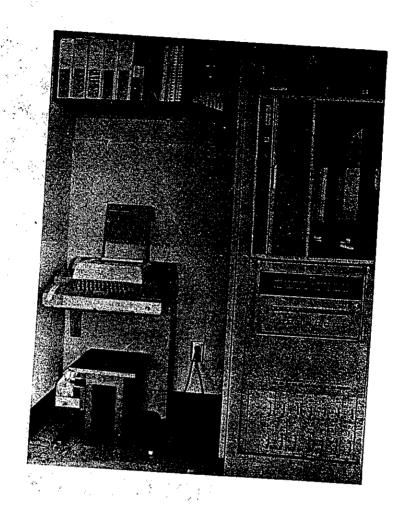


SCALE LEVELING FRAME IN ROUGH SCALE PIT

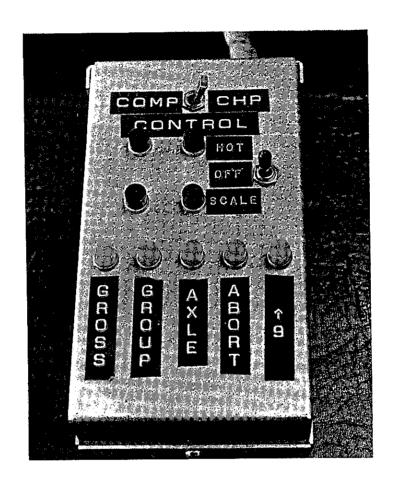
Figure 15



FINISHED SCALE PLATFORMS



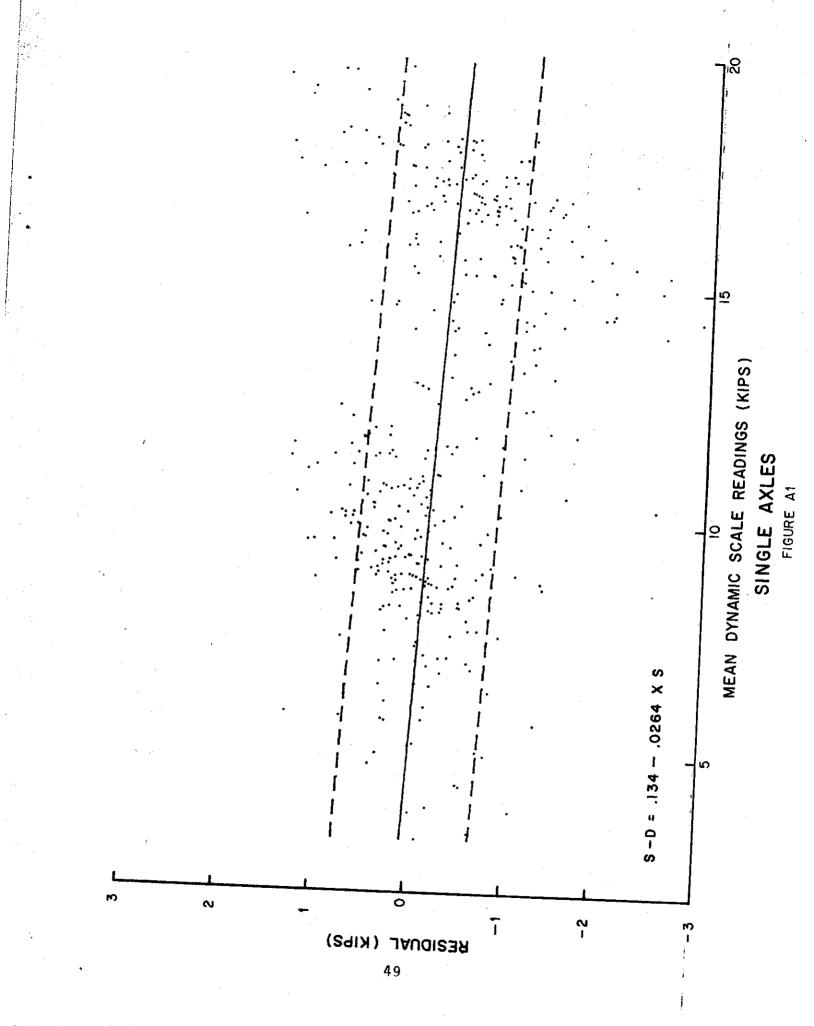
DYNAMIC WEIGHING COMPUTER CONTROL SHOWING TELETYPE PRINTER AT RIGHT AND MULTIPLEXER, TAPE DRIVE, COMPUTER AND SCALE POWER SUPPLIES AT LEFT

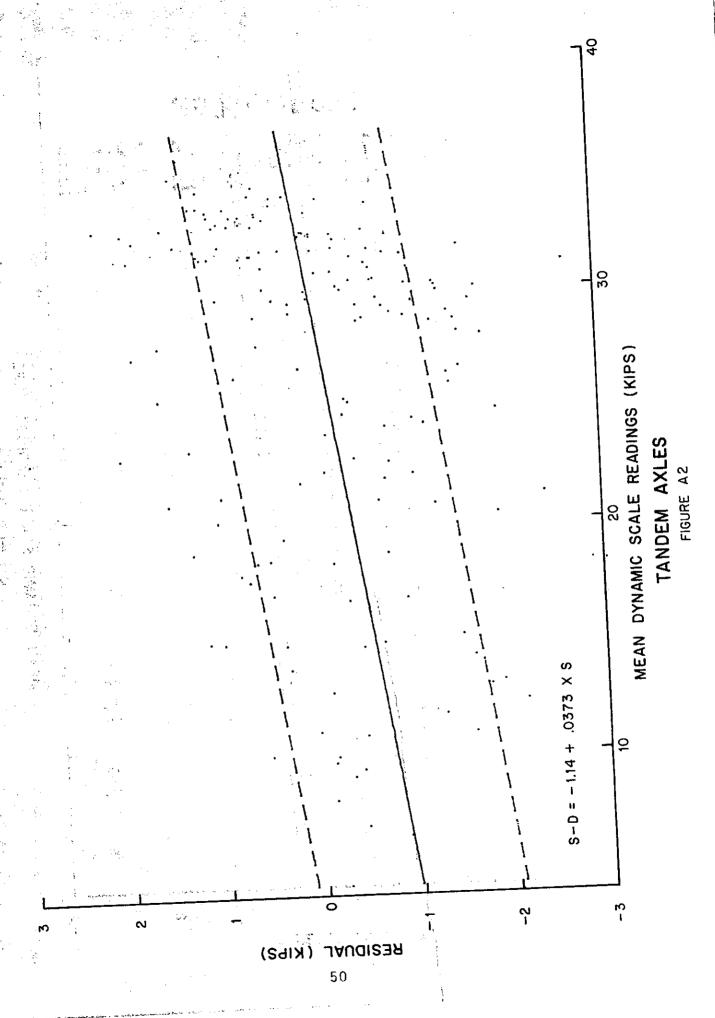


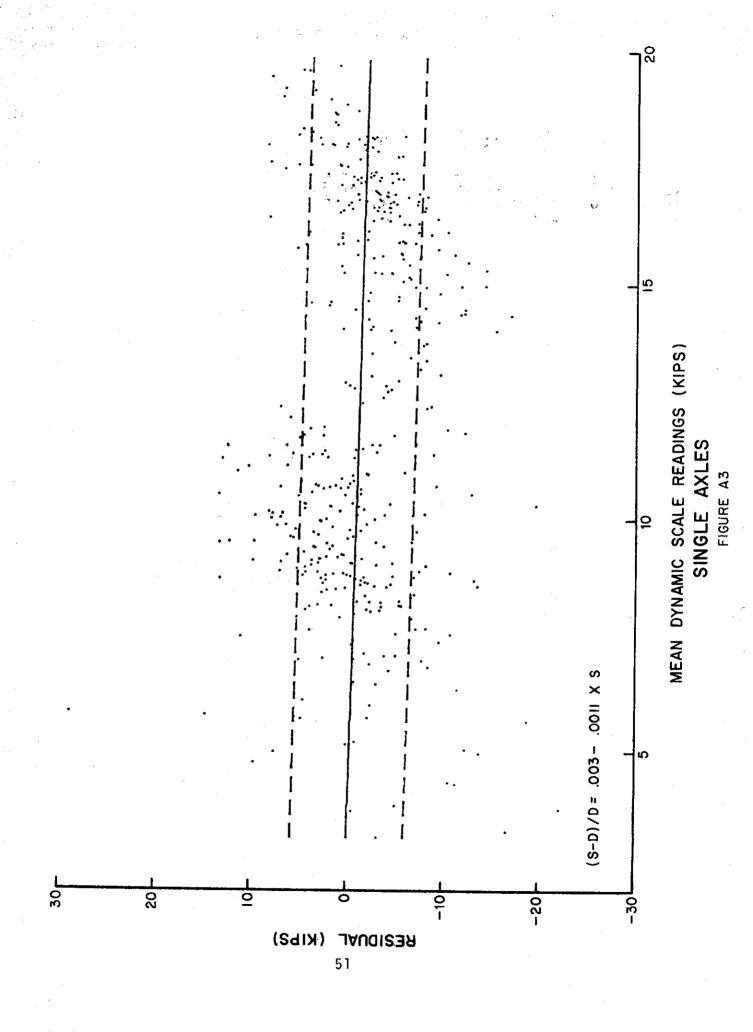
SCALEMASTER CONTROL BOX WITH MANUAL DIRECTIONAL SIGNAL SELECTION AND VIOLATION INDICATORS

## APPENDIX

h. 44 A. (\*\*)







#### NO. SCALES, SCALE NUMBERS 76 1 2 3 4 5 6

XBAR = 12	048E-2 .4848 92264E-1	,	SSX =	11136 7004.69 .350776	<b>,</b>
CRITICAL : PROB	20 KIP VA SCALE	LUES:	MEAN	KIPS	
P.100 = P.050 = P.005 = P.001 =	16.63	nes e	18.44 18.01 17.19 16.89 16.27	03 15 13	
FOR F.100	•				
ACTI LEGAL		•	- 1	CALCUI LEGAL	
402 27 429	0 0	PASS STOP TOTAL	27	399.9 19.7 419.6	2.1 7.3 9.4
FOR P.050	:		• . •	i	
ACT LEGAL				CALCUI LEGAL	
389 40 429	0 0 0	PASS STOP TOTAL	40	387.9 31.7 419.6	1.1 8.3 9.4
FOR F.010	:	A	•		
ACT LEGAL	UAL. VIOL.			CALCU LEGAL	
349 80 429	0 0 0	PASS STOP TOTAL	80	348.8 70.8 419.6	.2 9.2 9.4
FOR P+005	:		•		
ACT LEGAL	UAL. VIOL.	<u>\$</u>		CALCU LEGAL	LATED VIOL.
329 100 429	0	PASS STOP TOTAL	100	328.9 90.6 419.6	•1 9•4 9•4
FOR F.001	. :				
ACT LEGAL	UAL VIOL.	enio e		CALCU LEGAL	VIOL.
308 121 429	0	PASS STOP TOTAL		308.0 111.6 419.6	.0 9.4 9.4

NO. SCALES	Secale	NUMBERS?5	2 3 4 5	6
XBAR = 12.	75513E 4986 0901E-	SSX	A MLALM.	17
CRITICAL 2 PROB	O KIP SCAL		N KIPS	
P.100 = P.050 = P.010 = P.005 = P.001 =	18.2 17.7 16.9 16.6 16.0	3 18. 3 17. 7 16.	4501 0202 2019 9054 2923	
FOR P.100:				
ACTU LEGAL (	AL VIOL.		CALCL LEGAL	LATED VIOL.
404 25 429	0 0 0	PASS 404 STOP 25 TOTAL 429	401.8 17.3 419.1	2.2 7.7 9.9
FOR P.050:		·	·	
ACTUA LEGAL (	IOL.		CALCU LEGAL	
390 39 429	0	PASS 390 STOP 39 TOTAL 429	388.8 30.3 419.1	1.2 8.7 9.9
FOR P.010:	•			
ACTUA LEGAL V	L IOL.		CALCUL LEGAL	ATED VIOL.
353 76 429	0 0 0	PASS 353 STOP 76 TOTAL 429	352.7 66.3 419.1	•3 9•7 9•9
FOR P.005:				
ACTUAI LEGAL V:	COL.		CALCUL LEGAL	ATED VIOL.
331 98 429	0 0 0	PASS 331 STOP 98 TOTAL 429	88.2	9.8 9.9
FOR P.001:	9 W	i de la companya de La companya de la co		
ACTUAL LEGAL VI	OL.	· · · · · ·	CALCUL LEGAL	ATED VIOL.

PASS 308 STOP 121 TOTAL 429

•0 9•9 9•9

308.0 111.1 419.1

308 121 429

0

0

#### NO. SCALES, SCALE NUMBERS74 2 3 4 6 B1 = -.423414E-3BO = -.123508E-1SSX = 6987.48 MSE = .389727E-2 XBAR = 12.4036 SYX = .624281E-1 CRITICAL 20 KIP VALUES: MEAN KIPS SCALE PROB 17.99 18.3565 F.100 = 17.54 17.8939 P.050 = 17.0205 16.69 P.010 = 16.7124 16.39 P.005 = P.001 = 16.0554 15.75 FOR P+100: ACTUAL CALCULATED LEGAL 'VIOL. LEGAL VIOL. 0 PASS 398 396.2 1.8 0 STOP 31 21.3 9.7 0 TOTAL 429 417.4 11.6 398 31 429 FOR P.050: ACTUAL CALCULATED LEGAL VIOL. LEGAL VIOL. 0 PASS 387 385.9 1.1 0 STOP 42 31.5 10.5 385.9 387 0 STOP 42 31.5 10.5 0 TOTAL 429 417.4 11.6 42 429 FOR F.010: ACTUAL CALCULATED LEGAL VIOL. LEGAL VIOL. 0 FASS 348 347.8 .2 348 348 0 81 0 429 0 STOP 81 69.6 11.4 TOTAL 429 417.4 11.6 FOR F.005: CALCULATED ACTUAL LEGAL VIOL. LEGAL VIOL. 328 0 PASS 328 327.9 .1 101 0 STOP 101 89.5 11.5 429 0 TOTAL 429 417.4 11.6

ACTUAL CALCULATED LEGAL VIOL.

302 0 PASS 302 302.0 .0
127 0 STOP 127 115.4 11.6
429 0 TOTAL 429 417.4 11.6

#### NO. SCALES, SCALE NUMBERS?3 2 4 6

MO: acurea	7 0 W M M M M	Onpulato a	T W	
BO =2 XBAR = 12. SYX = .67	5509	SSX =	:25212 : 7187.24 : .455135	ì
CRITICAL 2 PROB	O KIF VA SCALE	MEAN	KIPS	<b>.</b>
P.100 = P.050 = P.010 = P.005 = P.001 =	18.12 17.63 16.71 16.38 15.69	16.48	ī33 23 394	
FOR F.100	;	•		
ACTU LEGAL			CALCUI LEGAL	
394 35 429	0 0 0	PASS 394 STOP 35 TOTAL 429	391.5 24.9 416.3	2.5 10.1 12.7
FOR P.050	•			
ACTI LEGAL		. •	CALCU LEGAL	
375 54 429	0 0 0	PASS 375 STOP 54 TOTAL 429	373.9 42.5 416.3	11.5
FOR P.010	<b>:</b>			
	UAL VIOL.	 	CALCU LEGAL	
337 92 <b>429</b>	0 0 0	PASS 337 STOP 92 TOTAL 429	79+5	12.5
FOR P+005	<b>:</b>			
ACT LEGAL	VIOL.		CALCU LEGAL	VIOL.
318 111 429	0, 0 0	PASS 318 STOP 111 TOTAL 429	317.9 98.4 416.3	
FOR P.001	<b>‡</b>			
	UAL VIOL.			JLATED VIOL.
293 136 429	0	PASS 293 STOP 136 TOTAL 429	293.0 123.4 416.3	
				<b>3</b> 5

## NO. SCALES, SCALE NUMBERS?2 2 6

B0 = .161995E-1 B1 = .266508E-4 XBAR = 12.8241 SSX = 7488.69 SYX = .767111E-1 MSE = .588459E-2CRITICAL 20 KIP VALUES: MEAN KIPS PROB SCALE 1.00 P.100 = 18.36 P.050 = 17.8 P.010 = 16.75 P.005 = 16.37 P.001 = 15.58 18.0586 17.5081 16,4757 16, 1021 15.3254 FOR P.100: ACTUAL LEGAL VIOL. CALCULATED LEGAL VIOL. 387 0 PASS 387 384.3 2.7 42 0 STOP 42 30.6 11.4 429 0 TOTAL 429 414.9 14.1 FOR P.050: ACTUAL SERVICE CALCULATED LEGAL VIOL. 367 0 PASS 367 365.7 1.3 62 0 STOP 62 49.3 12.7 429 0 TOTAL 429 414.9 14.1 FOR P.010: ACTUAL CALCULATED LEGAL VIOL. CALCULATED 322 0 FASS 322 321.8 .2 107 0 STOP 107 93.1 13.9 429 0 TOTAL 429 414.9 14.1 FOR P. 0051 ACTUAL LEGAL VIOL. CALCULATED LEGAL VIOL. 308 0 PASS 308 307.9 .1 121 0 STOP 121 107.0 14.0 429 0 TOTAL 429 414.9 14.1 FOR P.001: ACTUAL COMPANY CALCULATED LEGAL VIOL. 287 O PASS 287 287.0 .0 142 O STOP 142 128.0 14.0 0 TOTAL 429 414.9 14.1 429

NO. SCAL	ES, SCALI	E NUMBERS?6	1234	5 6
BO ==	1.14303	Y's 41	***********	
	5.9463	SSX	<b>≈</b> ∗3731.	
	•08706	MSE	= 10605 = 1.181	
			T+1010	(1) Y
CRITICAL	34 KIP	VALUES:		
PROB	SCAL	.E MEA	N KIPS	
P* J A A			<b>V</b>	
P.100 = P.050 =	32.6		5939	
	32.2	32.	1992 4579	
P.010 = P.005 =	31.4	31.	4579	
P.001 =	31.2 30.6			•
1.4001	_ av+c	30.0	5204	
FOR P.100	n.t			
ÁC	TUAL			11
	VIOL.		CALCL	LATED
	•		LEGHL	VIOL.
140	0	PASS 140	138.9	
25	6	STOP 31	19.7	
165	6	TOTAL 171	158.6	
		7	***************************************	T 45. 4 M
FOR P.050	);			
ACT	'UAL		CALCU	LATED
LEGAL.	VIOL.		LEGAL	
		• '.		
130	Ō	PASS 130	129.6	. 4
35	6	STOP 41	29.0	12.0
165	ద	TOTAL 171	158.6	12.4
FOR P.010	•			
1011 14010	•			
ACT	HAI			
LEGAL			CALCU	
			LEGAL	ATOL.
112	O	PASS 112	112.0	
53	6	STOP 59	46.6	12.4
165	6	TOTAL 171	158.6	12.4
				4. A. + "Y
FOR F.005	:			
A #1 144 .				
ACTI LEGAL			CALCUL	
I C. C) [4] [	VIOL.		LEGAL	VIOL.
111	^	MAMM		
54	0 6	PASS 111	111.0	• 0
165		STOP 60 TOTAL 171	47.6	12.4
m w w		TOTAL 171	158.6	12.4
FOR P.001:	}		•	
			-	
ACTL	JAL.	÷	CALCUL	ATED
LEGAL	VIOL.			VIOL.
		••	one took to f f f f f f f f f f f f f f f f f f	v sh Wilm ♦
105	0	PASS 105	105.0	.0
60	6	STOP 66	53.4	12.4
165	6	TOTAL 171	158.6	12.4
		•		

### NO. SCALES, SCALE NUMBERS?5 2 3 4 5 6

B0 = -1.05758 B1 = .30879E-1 XBAR = 25.8621 SSX = 10476.7 SYX = 1.05753 MSE = 1.11837 CRITICAL 34 KIP VALUES: PROB SCALE MEAN KIPS 

 P.100 =
 32.58
 32.6315

 P.050 =
 32.18
 32.2439

 P.010 =
 31.44
 31.5267

 P.005 =
 31.16
 31.2554

 P.001 =
 30.6
 30.7127

 FOR F.1001 ACTUAL LEGAL VIOL. CALCULATED LEGAL VIOL. 141 0 FASS 141 139.9 1.1 24 6 STOP 30 18.6 11.4 165 6 TOTAL 171 158.5 12.5 FOR P.050: ACTUAL CALCULATED ACTUAL LEGAL VIOL. LEGAL VIOL+ 0 PASS 131 6 STOP 40 6 TOTAL 171 130.6 .4 27.9 12.1 158.5 12.5 131 34 165 FOR P.010: ACTUAL CALCULATED LEGAL VIOL. 116 0 PASS 116 115.9 .1 49 6 STOP 55 42.5 12.5 165 6 TOTAL 171 158.5 12.5 FOR P.005: ACTUAL CALCULATED LEGAL VIOL. 111 0 FASS 111 54 6 STOP 60 165 6 TOTAL 171 111.0 47.5 12.5 158.5 12.5 FOR F.001: ACTUAL LEGAL VIOL. CALCULATED LEGAL VIOL. 106 0 PASS 106 106.0 .0 59 6 STOP 65 52.5 12.5 165 6 TOTAL 171 158.5 12.5

#### NO. SCALES, SCALE NUMBERS74 2 3 4 6

TOTAL CONTINUES	) (J) (J) [] (L) [L) [L) [L)	(C) ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	, 1 A	G 4 G	
BO =9 XBAR = 25. SYX = 1.0	6645		SSX =	.20938 10266. 1.1098	5
CRITICAL 3 PROB	4 KIP VI SCALE		MEAN	KIPS	
P.100 = P.050 = P.010 = P.005 = P.001 =	32.32 31.93 31.19 30.92 30.37		32.63 32.25 31.53 31.26 30.72	53 08 65	
FÖR F.100:					
ACTU LEGAL	AL VIOL.		ž	CALCU LEGAL	
141 24 165		STOP	30	140.0 19.1 159.1	10.9
FOR P.050:					
ACTU LEGAL				CALCU LEGAL	
133 32 165	0 6 6	PASS STOP TOTAL	133 38 171	132.5 26.6 159.1	.5 11.4 11.9
FOR P.010:					
ACTL LEGAL				CALCU LEGAL	LATED VIOL.
115 50 165	6 6	STOP	115 56 171	114.9 44.2 159.1	•1 11•8 11•9
FOR P.005	:				
ACTU LEGAL	VIOL.		yoğ m‡	CALCU LEGAL	LATED VIOL.
109 56 165	0	PASS STOP TOTAL	109	109.0 50.1 159.1	.0 11.9 11.9
FOR P.001	:	.*	* .		
. ACTU LEGAL					VIOL.
106 59 165	0 6 6	PASS STOP TOTAL	65		11.9

#### NO. SCALES, SCALE NUMBERST3 2 4 6

· · · · · · · · · · · · · · · · · · ·	oomer kondekt	D:3 2 4 6	
BO =98 XBAR = 25.8 SYX = 1.13	1.65	B1 = .265 SSX = 1035 MSE = 1.29	51.5
CRITICAL 34 PROB	KIP VALUES: SCALE	MEAN KIPS	· · · · · · · · · · · · · · · · · · ·
P.100 = P.050 = P.010 = P.005 = P.001 =	32.4 31.97 31.17 30.88 30.28	32.5299 32.1113 31.3326 31.0503 30.4662	
FOR P.100:			•
ACTUAL LEGAL VI	OL.		CULATED L VIOL.
142 23 165	O PASS 6 STOP 6 TOTAL	29 17.	2 11.8
FOR P.0501			
ACTUAL LEGAL VI		CAL LEGA	CULATED L VIOL.
133 32 165	O PASS 6 STOP 6 TOTAL	്വന ഫ്യ∔ം	4 .6 6 12.4 0 13.0
FOR F.010:			
ACTUAL LEGAL VI		CALI LEGAI	CULATED VIOL.
112 53 165	O PASS 6 STOP 6 TOTAL	59 46.0	13.0
FOR P.005:			
ACTUAL LEGAL VI	<b>OL.</b> •	LEGAL	CULATED VIOL.
108 57 165	6 STOP	108 108.0 63 50.0 171 158.0	13.0
FOR P.001:			
ACTUAL LEGAL VI	1. (A - 44 - 44) DL •	CALC LEGAL	CULATED VIOL.
102 63 165	6 STOP	02 102.0 69 56.0 71 158.0	13.0

#### NO SCALES, SCALE NUMBERS?2 2 6

•				_
BO = -1.387 XBAR = 26.424 SYX = 1.207	<b>4 1</b> .	SSX = 1	.639636E- L1164.9 L.45778	- 1.
CRITICAL 34 PROB	KIP VAL SCALE	UES: MEAN K	IFS	
P.050 = P.010 = P.005 =	33.18 32.7 31.82 31.5 30.84	32.444 31.995 31.171 30.872 30.254	5 8 3	
FOR P.100:				
ACTUAL LEGAL VI			CALCULA LEGAL \	TED TOL.
141 24 165	0 6 6	PASS 141 STOP 30 TOTAL 171	139.5 17.2 156.8	1.5 12.8 14.2
FOR P.050:				
ACTUA	L IOL•		CALCUL LEGAL	ATED VIOL.
126 39 165	0 6 6	PASS 126 STOP 45 TOTAL 171	125.6 31.2 156.8	.4 13.8 14.2
FOR F.010:				
ACTUA	AL ZIOL+		CALCUL LEGAL	ATED VIOL+
111 54 165	0 6 6	FASS 111 STOP 60 TOTAL 171	110.9 45.8 156.8	.1 14.2 14.2
FOR P.005:			•	
ACTU LEGAL		·	CALCU LEGAL	LATED VIOL.
107 58 165	0 6 6	PASS 107 STOP 64 TOTAL 171	107.0 49.8 156.8	14.2
FOR P.001				
ACTI LEGAL	JAL VIOL.	•	CALCU LEGAL	JLATED VIOL.
99 66 165	0 6 6	PASS 99 STOF 72 TOTAL 171	57+8	14.2

## FOR SCALES 1 2 3 4 5 & 6

#### FOR P. 100:

ACTI LEGAL	VIOL.		CALCI LEGAL	ULATED VIOL.
115 42 157	9 5 5	STOP 47	113. 7 35. 6	1. 3 11. 4 12. 7
FOR P. 050:				
ACTU LEGAL 102	VIOL.		CALCU LEGAL	LATED VIOL.
	Ø 5 5	STOP 50	47.0	
FOR P.010: ACTUR LEGAL V	;   <b>L</b>	÷	CALCUL	.ATED
82	4	į į	LEGAL	VIOL.
75 157	5	PÁSS 82 STOP 80 TOTAL 162		
FOR F. 905:				
	OL.	2	CALCULI LEGAL	ATED VIOL.
78 79 157		PASS 78 STOP 84 TOTAL 162		

#### FOR P. 001:

ACT LEGAL	VAL VIOL			CALCU LEGAL	LATED VIOL
73 84 1 <b>5</b> 7	9 5 5	PASS STOP TOTAL	73 89 162	73. 0 76. 3 149. 3	0. 0 12. 7 12. 7

ACT	UAL			LATED	
LEGAL	VIOL.	•		LEGAL	VIOL.
119 38 157	0 5 5	PASS STOP TOTAL	43	117. 4 31. 0 148. 4	1. 6 12. 0 13. 6

#### FOR F. 050:

ACTUAL					CALCU	Loten
	LEGAL	VIOL.			LEGAL	VIOL.
	103	9	PASS :		102. 4	Ø. 6
	54 157	5 5	STOP TOTAL :	59 162	46. 0 148. 4	13. 0 13. 6

#### FOR P. 010:

ACTUAL					CALCU	I ATEN
	LEGAL	VIOL.			LEGAL	VIOL.
	85	ø	PASS	85	84. 9	0. 1
•	72	5	STOP	77	63. 5	13. 5
	157	5	TOTAL	162	148. 4	13. 6

#### FOR P. 005:

ACTUAL				CELCU	LATED
LEGAL	VIOL.			LEGAL	VIOL.
78 79 157	8 5 5	PASS STOP TOTAL	78 84 162	78. 0 70. 4 148. 4	0. 0 13. 6 13. 6

#### FOR P.001:

HCT	UAL			CALCULATED		
LEGAL	VIOL.		•	LEGAL	VIOL.	
73 84 157	Ø 5 5	PASS STOP TOTAL	89	73. 0 75. 4 148. 4	0. 0 13. 6 13. 6	

#### FOR SCALES 2 3 4 & 6

#### FOR P. 100:

ACTUAL				CALCU	LATED
LEGAL	VIOL.	.*		LEGAL	VIOL.
116 41 157	ø 5 5	PASS STOP TOTAL	46	114. 7 32. 8 147. 5	1. 3 13. 2 14. 5

#### FOR P. 050:

. <i>(</i> ) -	ACTUAL LEGAL VIOL				CALCU LEGAL	
	53	5	PASS STOP OTAL	58	103. 5 44. 0 147. 5	0, 5 14, 0 14, 5

#### FOR P. 010:

ACTUAL				CALCU	LATED
LEGAL				LEGAL	VIOL.
83	8	PASS	83	82. 9	<b>0</b> . <b>1</b>
74	5	STOP	79	64. 5	14. 5
157	5	TOTAL	162	147. 5	14. 5

#### FOR P. 005:

ACTUAL	41		CULATED VIOL.
78		78 78.6 84 69.5	8. 9. 5 14. 5

#### FOR P. 001:

ACTUAL					CALCU	LATED
Ĺ		VIOL.			LEGAL	VIOL.
• -			14.0			
٠,	70	0	PASS	70	70. 0	0.0
1	87	5	STOP	92	77. 5	14. 5
. *	157	5	TOTAL	162	147. 5	14. 5

ACT	UAL			CALCU	LATED
LEGAL	VIOL.			LEGAL	VIOL.
114	ø	PASS	114	112. 4	1. 6
43	5	STOP	48	32. 8	<b>1</b> 5. 2
157	5	TOTAL	162	145. 1	16. 9

#### FOR P. 050:

: ACTUAL			•	CALCU	LATED
L	.EGAL	VIOL.	- \$	LEGAL	VIOL.
٠.	.1		w the second		
	98	ø	PASS 98	97. 6	9.4
m.	59	· 5	STOP 64	47. 5	16. 5
n É	157	์ ธิ	TOTAL 162	1,45. 1	16. 9

#### FOR P. 010:

ACT	UAL			CALCU	LATED
LEGAL	VIGE.			LEGAL	VIOL.
88	Ø	PASS	80	79. 9	0. 1
77	5.	STOP	82	<i>6</i> 5. 2	16. 8
157	5	TOTAL	162	145. 1	16. 9

#### FOR P. 005:

ACTUAL				CALCULATED	
LEGAL	VIOL.			LEGAL	VIOL.
77	ø	PASS	77	77. 0	ø. ø
89	, 5	STOP	85	68. 1	<b>16</b> . 9
157	5	TOTAL	162	145. 1	16.9

#### FOR F. 001:

ACTUAL				CALCULATED		
	LEGAL	VIOL.			LEGAL	VIOL.
	69	ø	PASS	69	69. Ø	ø. ø
	88	5	STOP	93	76. 1	16. 9
	157	· 5	TOTAL	162	145 1	16.9

## FOR SCALES 2 & 6

#### FOR P. 100:

ACTUAL				CALCULATED		
LEGAL	VIOL.			LEGAL	VIOL.	
108	e.	PASS	108	106. 8	1. 2	
49	5	STOP	54	37. 7	<b>16</b> . 3	
157	5	TOTAL	162	144. 5	17. 5	

#### FOR P. 050:

ACTUAL		4		CALCU	: CALCULATED		
LEGAL	VIOL.			LEGAL	VIOL.		
3 W 1 3 4 5							
89	Ø	PASS	89	. 88. 6	0.4		
68	5 :	STOP	73	· 55. 8	17. 2		
157	5	TOTAL	162	144. 5	17. 5		

#### FOR P. 010:

ACTUAL				CALCULATED	
LEGAL	VIOL.			LEGAL	VIOL.
76 81 157	0 5 5	PASS STOP TOTAL	76 86 162	76. 0 68. 5 144. 5	0. 0 17. 5 17. 5

#### FOR P. 005:

	ACT	UAL			CALCU	LATED
L	EGAL	VIOL.			LEGAL	VIOL.
	<b>73</b> %.	. 0	PASS	73	73. 0	Ø. Ø
673	84	, 5	STOP	89	71. 5	17. 5
	157	5	TOTAL	162	144. 5	17. 5

#### FOR P. 001:

HCTORL				CALCU	LATED
LEGAL	VIOL.			LEGAL	VIOL.
5. 4	s := 1	:			
66	8	PASS	66	66. 0	9. 9
91	5 .	STOP	96	78. 5	17. 5
157	5	TOTAL	162	144. 5	17.5

		CHLCULHTED				
		LEGAL	VIOL.			
PASS	1878	1871. 8	6. 2			
STOP	142	105. 2	36. 8			
TOTAL	2020	1976. 9	43. 1			

#### FOR P. 050:

		CHECHENIED				
		LEGAL		VIOL		
	1838	1834.	_	3.	_	
STOP	182	142.	4	39.	6	
TOTAL	2020	1976.	3	43.	1	

#### FOR P. 010:

	CALCULATED			)
	LEGF	ìL.	Alor	
1735	1734.	5	Ø.	5
285	242.	4	42.	6
2020	1976.	9	43.	1
	285	LEGF 1735 1734. 285 242.	LEGAL 1735 1734.5 285 242.4	LEGAL VIOL 1735 1734.5 0. 285 242.4 42.

#### FOR P. 005:

		LEGAL	VIOL.
PASS	1704	1703. 8	0.2
STOP	316	273. 1	42. 9
TOTAL	2020	1976. 9	43. 1

#### FOR P. 001:

	LEGAL	VIOL.
 1628 392 2020	1628. 0 348. 9 1976. 9	0. 0 43. 1 43. 1

		CALCULATED			
-	7	LEGF	łL.	AIOF	
	1884 136 2020		8	6. 37. 43.	2

#### FOR F. 050:

	. CALCULATED	
	LEGAL	
PASS STOP TOTAL	 1833. 0 143. 4 1976. 4	3. 0 40. 6 43. 6

#### FOR P. 010:

	CALCULATED	
	LEGAL	. VIOL.
1731 289 2020	1730. 6 245. 6 1976. 4	3 43.2

### FOR P. 005:

•	ton ton half year	ATOF.
PASS 1704 : STOP 316 TOTAL 2020 :	1,703, 8 272, 6 1976, 4	

#### FOR P. 001:

PASS 1638 STOP 382	LEGAL	VIOL.	
	 1638. 0 338. 5	0. 0 43. 5	
	 1976. 4	43. 5 43. 6	

CALCULATED

CALCULATED LEGAL VIOL.

PRSS 1878 1871 7 6.3 STOP 142 103.3 38.7 TOTAL 2020 1975.0 45.0

FOR P. 050:

CALCULATED LEGAL VIOL.

PRSS 1830 1827.0 3.0 STOP 190 147.9 42.1 TOTAL 2020 1975.0 45.0

FOR P 010:

CALCULATED
LEGAL VIOL

PRSS 1724 1723. 6 0. 4 STOP 296 251. 4 44. 6 TOTAL 2020 1975. 0 45. 0

FOR P. 005:

CALCULATED LEGAL VIOL

PRSS 1696 1695.8 0.2 STOP 324 279.2 44.8 TOTAL 2020 1975.0 45.0

FOR P. 001:

CALCULATED

PRSS 1626 1626.0 0.0 STOP 394 349.0 45.0 TOTAL 2020 1975.0 45.0

CALCULATED LEGAL VIOL.

PASS 1876 1868.3 7.7 STOP 144 101.8 42.2 TOTAL 2020 1970.1 49.9

FOR P. 050:

CALCULATED
LEGAL VIOL.

PASS 1810 1807 1 2.9 STOP \* 210 163.1 46.9 TOTAL 2020 1970.1 49.9

FOR P. 010:

CALCULATED
LEGAL VIOL.

PASS 1714 1713.5 0.5 STOP 306 256.7 49.3 TOTAL 2020 1970.1 49.9

FOR P. 005:

the following section

CALCULATED
LEGAL VIOL

PASS 1680 1679.7 0.3 STOP 340 290.4 49.6

TOTAL 2020 1970.1 49.9

FOR P. 001:

CALCULATED LEGAL VIOL

PASS 1602 1602.0 0.0 STOP 418 368.2 49.8 TOTAL 2020 1970.1 49.9

CALCULATED LEGAL VIOL.

PRSS 1851 1843.1 7.9 STOP 169 121.8 47.2 TOTAL 2020 1964.9 55.1

FOR P. 050:

CALCULATED LEGAL VIOL.

PASS 1787 1783.6 3.4 STOP 233 181.3 51.7 TOTAL 2020 1964.9 55.1

FOR P: 010:

CALCULATED LEGAL VIOL.

PASS 1680 1679.5 0.5 STOP 340 285.4 54.6 TOTAL 2020 1964.9 55.1

FOR P. 005:

CALCULATED LEGAL VIOL.

PASS 1647 1646.8 0.2 STOP 373 318.2 54.8 TOTAL 2020 1964.9 55.1

FOR P. 001:

CALCULATED LEGAL VIOL.

PASS 1571 1571.0 0.0 STOP 449 394.0 55.0 TOTAL 2020 1964.9 55.1